

Introductory Invited Paper

# Gate dielectric breakdown in the time-scale of ESD events

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## Abstract

Transmission line pulse (TLP) measurements are used to demonstrate that oxynitride breakdown projections from DC measurements using conventional area and voltage-scaling techniques can be extended to the nanosecond time-scale. ESD protection systems can thus be designed to prevent dielectric breakdown. Important concepts in gate dielectric breakdown such as the anode–hole injection model and area and statistical effects are discussed and applied to the nanosecond regime.

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## 1. Introduction

The challenge of electrostatic discharge (ESD) design is that as transistor scaling continues and operating voltages are lowered, the interface to the outside world and therefore the ESD specifications remain the same. Moreover, ESD protection has aimed at avoiding the first breakdown voltage for snapback of a transistor. However as has been highlighted by Duvvury and Amerasekera [1] this snapback voltage and the median breakdown voltage of the gate dielectric are converging (Fig. 1), making it difficult to ensure the robustness of gate dielectrics in an ESD event. This is particularly true for 1 V I/O's in high-speed, high-performance applications, where transistor gates may be directly connected to an external pin or NFETs may be used as compact decoupling capacitors between VDD and VSS, exposing the thin gate dielectric to ESD pulses which are charac-

terized by very high-current and very short duration. During an ESD pulse, the ESD protection and interconnects can both contribute voltage drops, and their sum must not be higher than the voltage which a dielectric can withstand.

A vast knowledge base exists for oxide breakdown in the long time-scale, and a few publications have addressed short time-scales [1–8]. For the most part, studies which described breakdowns at short times have used methodology developed for thicker oxides. In the case of thinner oxides or oxynitrides at voltages below  $\sim 5$  V, the voltage acceleration is no longer  $1/E$ , and small differences in thickness have a significant effect on the dielectric breakdown voltage. The theory which has emerged from thin oxide studies has not been applied before by the ESD community and statistical and area-dependent effects have generally been neglected. Therefore, the purpose of this paper is to study the relevance of long time-scale TDDB data in predicting the response to short time-scale ESD events, especially for sub-2 nm dielectrics in both NFETs and PFETs. A summary of important concepts for dielectric breakdown will be given and

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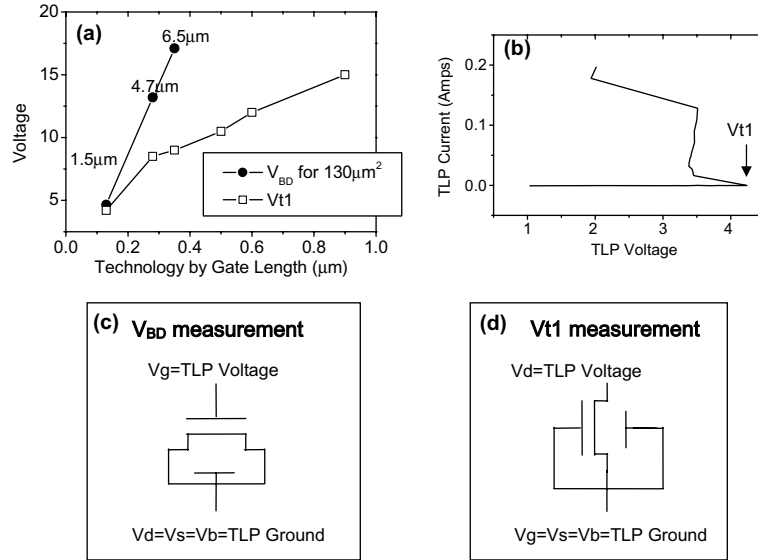


Fig. 1. (a) First breakdown voltage ( $V_{t1}$ ) for NFET snapback and dielectric breakdown voltage  $V_{BD}$  vs. gate length for several technology generations of NFETs. Both voltages were measured using a TLP system with 3 ns risetime and 100 ns pulses.  $V_{BD}$  measurements are also shown in Fig. 3. A measurement of  $V_{t1}$  is shown in (b) for a 1.5 nm oxynitride in a  $0.13 \times 2000 \mu\text{m}$  device.  $V_{t1}$  is sensitive to underlying doping as well as to channel length; (c) measurement configuration for  $V_{BD}$  and (d) for  $V_{t1}$ .

experimental results from studying 1.5–1.9 nm dielectric breakdown in the nanosecond regime will be presented. It will be shown that many of the breakdown concepts developed for the long time-scale continue to apply to the nanosecond regime. Methods for projection to thinner dielectrics (1.2 nm) will be discussed.

## 2. Background

Several important concepts will be used in the discussion of dielectric breakdown in the nanosecond regime. These concepts will be reviewed here before the new experimental results are presented.

### 2.1. Voltage acceleration

The anode–hole injection model and the validity of various approximations is treated extensively in Ref. [9]. A description of the model for  $V < 9 \text{ V}$  will be given here. A diagram to illustrate the process is shown in Fig. 2a. The picture for thin oxides is that as electrons tunnel across the oxide, some of those electrons create electron–hole pairs. A portion of those generated holes are injected from the anode back into the oxide and can tunnel across ( $J_h$ ). A fraction of those tunneling holes generate traps in the oxide. When the oxide is bridged by overlapping traps, we call it breakdown. The following equation describes the relationship between time to breakdown ( $T_{BD}$ ) and electric field in the anode–hole injection model.

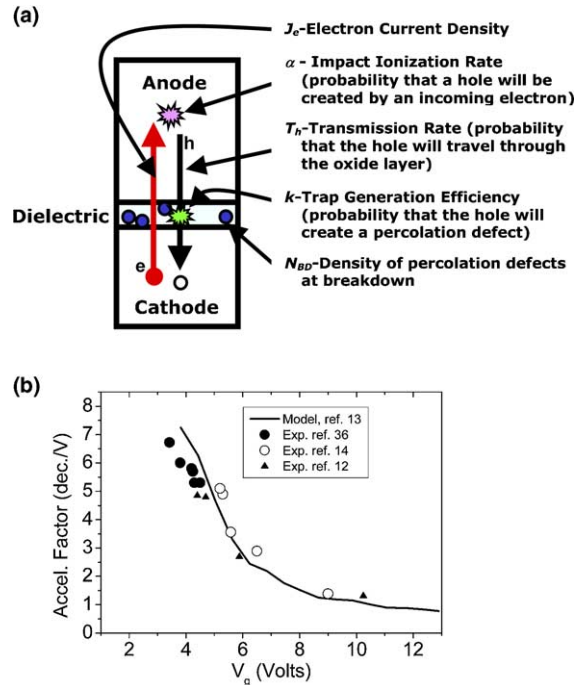


Fig. 2. (a) Illustration of the anode–hole injection model showing the various terms in Eq. (1). (b) Theoretical calculation of voltage acceleration factor for time to breakdown from Ref. [13] as well as experimental results from several groups [10,12,14].

$$T_{\text{BD}} = \left( \frac{N_{\text{BD}}}{k} \right)^{\frac{1}{m}} \frac{1}{J_{\text{h}}} \quad (1)$$

where  $N_{\text{BD}}$  is the critical trap density, a quantity that varies statistically and can be predicted from the percolation model which is explained in the following section. The statistical variation is independent of field. The lattice–hole interaction coefficient,  $k$ , indicates how difficult it is for a tunneling hole to generate a trap. Since the rate of trap generation may vary with stress time, the non-linearity coefficient,  $m$ , is included. The number of tunneling holes can be described by  $J_{\text{h}} = J_{\text{e}}\alpha T_{\text{h}}$ , where  $J_{\text{e}}$  is the density of tunneling electrons,  $\alpha$  is the probability of electron–hole pairs being generated, and  $T_{\text{h}}$  is the transmission probability of holes. When the electron tunneling is Fowler–Nordheim,  $J_{\text{e}} = A \exp(-B/E)$  where  $A$  and  $B$  are constants and  $E$  is the electric field. So  $\log(T_{\text{BD}}) \sim 1/E$  is valid at voltages where essentially all electrons which tunnel from the cathode generate electron–hole pairs in the anode ( $\alpha = 1$  or has no field-dependence) and all of those generated holes tunnel back across the oxide ( $T_{\text{h}} = 1$  or has no field-dependence). In fact, in the range where this study has been performed, around 5 V, although the electron tunneling continues to be Fowler–Nordheim, both  $\alpha$  and  $T_{\text{h}}$ , depend on  $E$ . The time to breakdown equation is dominated by  $\alpha = M \exp(DV)$  where  $M$  and  $D$  are constants, and therefore  $\log(T_{\text{BD}}) \sim V$  as has been reported by many different groups [10–12]. Fig. 2b shows the voltage acceleration as a function of voltage plotted by Alam et al. [13] based on a theoretical evaluation of all of the terms considered above. Measurements from several groups are also included in Fig. 2b [10,12,14]. A further complication as the voltage is lowered below 4 V is that  $\alpha$  begins to depend even more steeply on voltage so that  $T_{\text{BD}} \sim V^{-44}$  as has been reported by Wu et al. [15]. This becomes important for projections to operating voltage, but not for nano–second time–scale breakdown for oxynitrides down to 1.2 nm.

## 2.2. Polarity dependence

We include the ESD response for both NFETs and PFETs because PMOS reliability for sub-2 nm oxynitrides is a particularly important topic [16]. Although PFETs are more robust in the 5–7 V range, the time to breakdown, at operating voltage, of PFETs is shorter than that of NFETs because minority ionization can occur in PFETs. This process creates an energetic hole, and although very rare, becomes significant at low voltages [17].

The measurements and validation discussed above are based on DC stress, unlike the ESD pulse of very short duration. Therefore, the fundamental question is whether or not the DC formulation is relevant for ESD breakdown. In this paper, we directly measure

breakdown in the ns regime. We confirm that the same acceleration rules can be used both in the DC and ns regimes.

## 2.3. Percolation model

For more than a decade, oxide breakdown results have been interpreted based on the percolation model. Many different groups have validated this model [18–22] and the data here will be interpreted based on this model. Some of the implications of the model will also be explored. The percolation model is as follows: Traps form randomly in space throughout the dielectric. As more and more traps are formed, the traps begin to overlap. When the overlapping traps bridge the dielectric, a high-current path (percolation path) forms between the two electrodes and breakdown occurs (Fig. 3). The percolation model accurately predicts the statistical variation observed in oxide breakdown data as well as the area-dependence [18]. The statistical variation in breakdown time or breakdown voltage simply means that if a number of identical dielectrics are stressed under identical conditions, statistically, percolation paths will form earlier in some than in others. Because the breakdowns follow a statistical pattern, the time for a small fraction of devices to exhibit breakdown can be predicted from the median time to breakdown and the Weibull shape factor [20]. In addition, increasing the sample area is similar to increasing the statistical pool and therefore results in a shorter breakdown time. The observed area-dependence of the breakdown time is correctly predicted by the percolation model [18].

## 2.4. Importance of statistics

Although most papers in the ESD field have focused on determining the median breakdown voltage of a dielectric, it is extremely important to take into account the statistical variation of breakdown and the area-dependence. As shown in Fig. 4 from Wu et al. [18], the Weibull shape factor decreases as oxide thickness

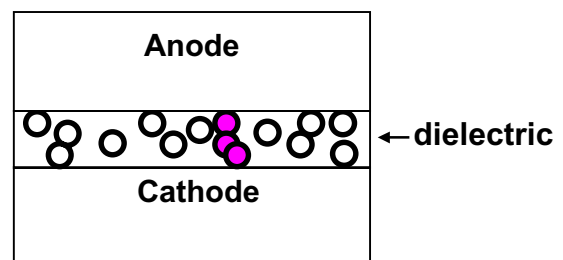


Fig. 3. Traps are depicted as circles within the dielectric. The traps which form a percolation path across the dielectric are shaded. The path may contain more than three traps depending on the arrangement.

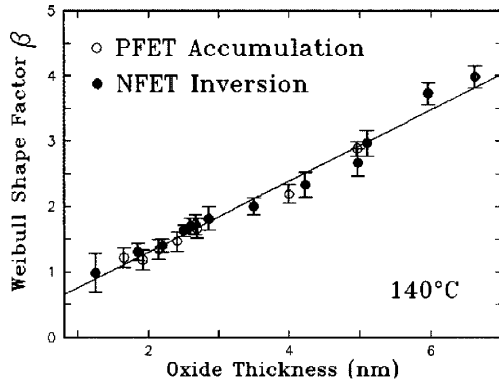


Fig. 4. Weibull shape factor vs. oxide thickness from Wu et al. [18] illustrating the concept that as the dielectric becomes thinner, the statistical spread in time to breakdown increases.

is reduced. The breakdown voltage is related to the Weibull shape factor,  $\beta$ , by the following equation:

$$\Delta V_{BD} = \frac{1}{\text{Volt. Acc.}} \times \frac{1}{\beta} \log \left( \frac{\ln(1 - f_1)}{\ln(1 - f_2)} \right) \quad (2)$$

The difference in breakdown voltage for a 5 nm oxide, as shown in Fig. 5, is almost 2 V. Although this effect is somewhat smaller for thinner oxides, since the voltage acceleration factor increases at these voltages, it still remains a >10% effect. While  $V_{t1}$  was much lower than  $V_{BD}$  (e.g. 0.3  $\mu\text{m}$  technology node  $V_{BD} - V_{t1} \sim 7$  V) statistical effects which changed  $V_{BD}$  by  $\sim 2$  V could be ignored. However, in the regime where  $V_{t1}$  is close to  $V_{BD}$ , these statistical effects can make the difference between a product passing the ESD specification or not. These statistical effects are taken into account in our study and included in the projection to 1.2 nm.

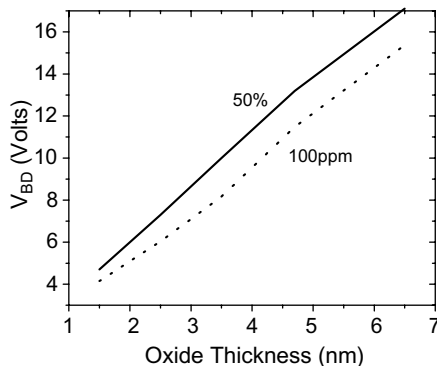


Fig. 5.  $V_{BD}$  vs. dielectric thickness for 100 ns stress on NFETS. The spread between the median value and a standard industry specification is shown. Measurements shown in Fig. 1a are used for the 50% line, and the conversion to 100 ppm use the Weibull shape factor values from Fig. 4.

## 2.5. Area-dependence

As described above, the breakdown time or breakdown voltage also depends on the area of the dielectric under test. The difference in breakdown voltage is shown in Eq. (3).

$$\Delta V_{BD} = \frac{1}{\text{Volt. Acc.}} \times \frac{1}{\beta} \log \left( \frac{A_1}{A_2} \right) \quad (3)$$

In oxide reliability studies, we use the area-dependence to relate the breakdown measured on a test structure, to the area of the entire chip. This is valid, because the stress voltage being considered is simply the operating voltage which will be applied all over the chip. In an ESD event, the voltages are more local, and the affected area may be similar to the tester area. However, there may be cases where the gate dielectric area affected by an ESD event may be more than an order of magnitude larger or smaller than the tester area and therefore the area-dependence is included in this work.

## 2.6. Soft breakdown

One topic which has been extensively studied recently, in connection with thin oxides, is soft breakdown [23–27]. This is when a percolation path is completed, but the thermal effects associated with traditional dielectric breakdown do not take place and the transistor remains functional. Soft breakdown occurs at low voltages, or when the current flowing through the oxide is limited by instrumental compliance or by a series resistance [23–25]. After soft breakdown, the current–voltage characteristic shows a power-law relationship ( $I = V^\delta$  with  $\delta = 4$ –7), whereas, hard breakdown results in an ohmic characteristic ( $\delta \sim 1$ ). Soft breakdown is not relevant for ESD events which cause breakdown in 1.2–1.9 nm oxynitrides, due to the breakdown voltage. Hard breakdown has been observed at voltages as low as 2 V [28]. Soft breakdown can occur at voltages above 4 V if current is limited [25], but high currents are certainly available in ESD events. Therefore, the conditions of low voltage and limited current do not apply to ESD events, and soft breakdown is not generally relevant to the topic.

## 2.7. Previous work in the short time-scale

A few papers, without considering ESD events, have included a discussion of the oxide breakdown transient, Ridley [3] calculated that breakdown should occur in approximately 10 ns. Experimentally, Lombardo et al. [29] recently stated that above 4 V, the breakdown transient is greater than  $10^5$  A/s. These studies indicate that a breakdown event could be completed within the time-scale of an ESD event. Below, a number of papers which consider oxide breakdown directly in the context of an ESD event are discussed.

Cheung [6] has demonstrated that the gate oxide degradation mechanism remains unchanged in the short time-scale. His work used an indirect measure of oxide damage developed in order to study plasma damage [6]. He obtained voltage acceleration factors matching the universal voltage acceleration curve in Fig. 2b as he compared damage due to nanosecond stresses and DC stresses. His paper is the first, to our knowledge, which includes an explanation of statistical and area-dependent effects in the context of oxide breakdown in an ESD event.

Matsuzawa et al. [7] studied a 3 nm oxide and showed that the breakdown mechanism was the same over the range of  $10^{-4}$  to  $10^{-7}$ s by using repeated TL pulses. They used an equation similar to our Eq. (1) to simulate the time to breakdown as a function of voltage and find good agreement for the 3 nm oxide. The lack of agreement between their data and the simulation for the 6 nm oxide remains a topic for further investigation. They also include a helpful discussion on the edge effects in a transistor.

Salman et al. [30] have studied the oxide robustness in an ESD event. They include a figure similar to our Fig. 1a) which compares oxide breakdown voltage with  $V_{t1}$  and holding voltage as a function of technology generation. They show an example of a circuit with a conventional snapback ESD protection system where the failure mode is oxide rupture although the median oxide breakdown voltage was slightly above  $V_{t1}$  for that technology (0.1  $\mu\text{m}$ ). For longer gate length protection structures, the differential resistance causes the holding voltage to exceed the oxide breakdown voltage at high ESD current. Consequently, oxide breakdown occurs in the gate drain overlap region of the protection NFET.

Wu and Rosenbaum [2] concluded that for a 2.2 nm oxide, the  $1/E$  dependence holds over the range of  $10^4$  to  $10^{-9}$  s. To our knowledge, this study covers the widest range of time to breakdown reported to date. They also show that self-heating effects are not important in understanding oxide breakdowns at these voltages and time-scales. PMOS devices in accumulation are studied, because accumulation stress has a lower  $V_{BD}$  for PMOS. In the voltage range they studied, the time to breakdown is expected to exhibit an approximately  $1/E$  dependence. However, as even lower voltages are probed, this  $1/E$  dependence, which comes from a simplification of the anode-hole injection model, no longer holds [9] as described above.

Additionally, they state that with sufficient guard-banding, statistical effects are not a point of concern [2]. Although this is certainly true, it becomes increasingly expensive in real estate and sometimes impossible to build large voltage margins into the ESD protection system. For example, if the median breakdown time of a given oxide is 4 V, in order to provide sufficient guard-banding, without calculating statistical effects,

the ESD protection system would have to be designed such that the voltage would never rise above 3 V. There is a significant advantage in doing the simple calculations outlined here to determine the area and statistical effects in order to see that the protection system must be designed to avoid 3.4 V, for example.

Our experiments are described in the following sections. We have focused on the aspects of dielectric breakdown most relevant to ESD design for current technologies. Both NFETs and PFETs with 1.5 nm oxynitrides are tested in inversion. Methodology for projection to even thinner dielectrics is discussed.

### 3. Experiment

#### 3.1. Transmission line pulse measurements

Transmission line pulse (TLP) testing has been used to study the effect of an electrostatic discharge [31]. Our TLP system applies 100 ns pulses (3 ns rise time) to a device, while measuring the voltage across and current through it. The robustness of gate dielectrics on a very short time-scale was investigated by subjecting them to incrementally increasing voltage pulses, and making DC leakage measurements between pulses, as depicted in Fig. 6. Testers of 0.13  $\mu\text{m}$  NFETs and PFETs with oxynitride dielectrics were designed specifically for this experiment. One contact pad was wired to the gate and another contact pad to the source, drain and tub to comply with the 2-probe TLP configuration. Series resistance was minimized by using multiple  $0.13 \times 10 \mu\text{m}$  devices so that metal contact to poly-silicon was never more than 5  $\mu\text{m}$  away. Testing in inversion also ensured that the resistance associated with a

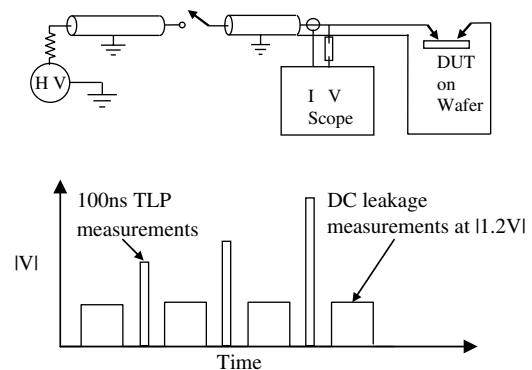


Fig. 6. Wafer-level transmission line pulse system used in these experiments. The 50  $\Omega$  environment is preserved down to within a few mm of the device using triaxial probes. The TLP system applies a 100 ns pulse during which voltage and current are measured. Between TLP pulses, a DC leakage measurement is performed.

substrate or *n*-well contact was not included. In a TLP system, the voltage and current levels depend on the relative impedance of the transmission line (TL) with respect to the device under test (DUT):  $I_{DUT} = V_C / (Z_{DUT} + Z_{TL})$  where  $V_C$  is the charging voltage. If a gate dielectric has a resistance  $Z_{DUT} = 10 \text{ k}\Omega$ , with  $V_C = 4.7 \text{ V}$  and  $Z_{TL} = 50 \Omega$ , the total resistance is dominated by the resistance of the DUT, so the stress is equivalent to a constant-voltage stress.  $V_{DUT}$  was measured to be within 0.1 V of  $V_C$  as further confirmation of minimal series resistance. We can therefore compare the results for the first dielectric breakdown under TLP stress to DC constant-voltage stress [32].

### 3.2. High resolution measurements of the breakdown event

Dielectric breakdown was directly observable in the TLP waveforms as shown in Fig. 7. The finer time-reso-

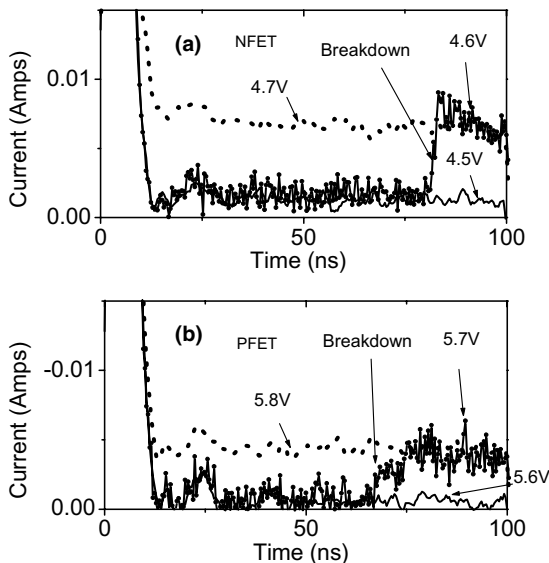


Fig. 7. TLP waveforms show dielectric breakdown with high-time resolution in (a) an NFET and (b) a PFET. The voltage steps before and after the step in which the first dielectric breakdown occurred are plotted. The observed increase in current (labeled “breakdown”) is accompanied by a decrease in voltage. After such an event, the DC leakage at  $|1.2 \text{ V}|$  increases to the  $\pm 1 \times 10^{-4} \text{ A}$  range. For pulses which showed no increase in current, a 5-point averaging routine was used to smooth the data to improve the clarity of these figures. The initially high-current value is an artifact of the high-frequency measurement and occurs because at the measurement location, the incident and reflected pulses do not overlap perfectly. Although a relatively fast breakdown transient is shown for the NFET and a slower transient shown for the PFET, no difference in average transient speed was detected between the two types of device. The breakdown transients from both NFETs and PFETs were in the 2–10 ns range.

lution used here confirms the finding of Lombardo et al. [29]. The breakdown event can occur in less than 2 ns and has a transient as high as  $3.5 \times 10^6 \text{ A/s}$ . The slope of the transient is similar for both 5 V and  $-6 \text{ V}$ , although transients at lower voltages may be significantly less steep [29]. If the breakdown transient were more than 100 ns, it is possible that the breakdown process would not have been completed within one stress cycle, resulting in significant differences between breakdown measured in the DC regime and that in the nanosecond regime. With this time-scale established for breakdown, we see no reason why the damage caused by a pulse which lasts 100 ns would not be similar in character to the damage caused by a longer stress. However, since some of the measured transients lasted several nanoseconds, if we had been measuring breakdown due to a 1 ns pulse, DC extrapolation may not have been possible. Since some ESD transients only last a few nanoseconds, further study is required, before the methods used here are extrapolated to the 1–2 ns regime. These data indicate that DC extrapolation techniques can be used at least for pulse widths of 10 ns or greater.

### 3.3. Ramped voltage measurements

We also assume that the bulk of the damage occurs in the final step of the ramp. For example, if a device undergoes hard breakdown within 100 ns at 4.8 V, using the voltage acceleration factor of 5.8 dec./V, we find that it would last 380 ns at the previous pulse of 4.7 V. Therefore, the damage at 4.7 V is only about 1/4 of that at 4.8 V, at 4.6 V it is only  $1/4n$  of that at 4.8 V (where  $n$  = number of steps between 4.6 and 4.8 V), and we can consider the main damage to occur in the final voltage step. To confirm the validity of this assumption, we have made measurements by repeatedly pulsing at the same voltage. The time to breakdown obtained from these measurements at 4.6 V and 4.7 V falls on the same voltage acceleration line as the ramped-voltage measurements as shown in Fig. 9. Although at higher voltages this assumption may not have held true, and the stress involved at each step of the ramp needed to be calculated in order to compare ramped voltage measurements and constant voltage measurements [33], it is sufficient to consider the final step of the ramp in this regime where the voltage acceleration is  $>5.8 \text{ dec./V}$ .

## 4. Results

### 4.1. DC vs. nanosecond measurements—voltage acceleration

Fig. 8 shows the data for  $0.13 \mu\text{m}$  NFETs and PFETs with 1.5 nm oxynitride gates. All dielectric breakdowns measured by TLP were hard ( $\delta = 1\text{--}2.5$  where  $I = V^\delta$ ).

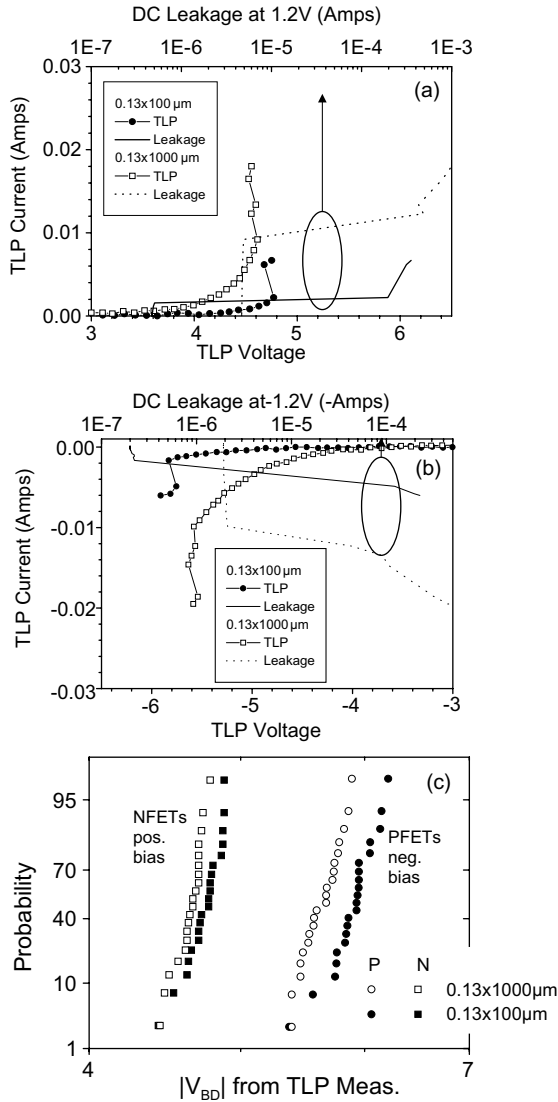


Fig. 8. TLP data showing 1.5 nm oxynitride breakdown (a) TLP current vs. TLP voltage for the two NFET areas (pos. voltage stress). DC leakage is shown on the top axis and is plotted against TLP current; (b) similar plot for PFETs (neg. voltage stress); (c) lognormal plot of  $|V_{BD}|$ , the point at which at least a 10x increase in DC leakage was observed. The 50% probability values are listed in Table 1. Two areas were tested for both NFETs and PFETs.

As shown, the leakage at 1.2 V (plotted on the top axis vs. TLP current) increases by several orders of magnitude at the point of breakdown. Although in many cases several dielectric breakdowns were observed, the voltage where first dielectric breakdown was observed was considered  $V_{BD}$ . We compared  $V_{BD}$  to our expectations based on DC measurements at lower voltages [34]. The voltage acceleration data are shown in Fig. 9 and agree with published values [10,35–37]. The voltage acceleration

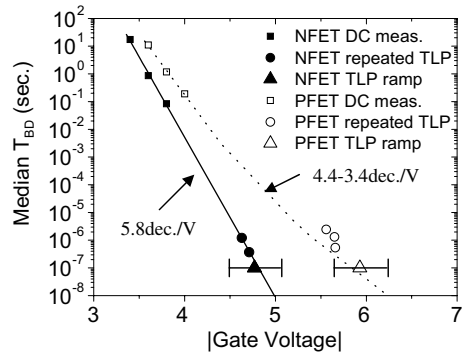


Fig. 9. DC constant voltage measurements [34] of time to breakdown for 1.5 nm oxynitrides are fit to determine the voltage acceleration. TLP measurements on  $0.13 \times 100 \mu\text{m}^2$  devices are plotted just below 100 ns. The overlap of the TLP measurement with the projection from DC measurements confirms that even nanosecond-range breakdowns can be predicted using standard projection techniques. In addition, median breakdown times from repeated 100 ns pulses at 4.6 and 4.7 V for NFETs and 5.65 and 5.55 V for PFETs are plotted, demonstrating that with this steep voltage acceleration, the bulk of the damage occurs in the final step of the ramp.

lines are extrapolated to the 100 ns range. The  $V_{BD}$  values from Fig. 8 are plotted with error bars and overlap the DC projections. Also, repeated TLP pulses at 4.6 and 4.7 V for NMOS and 5.5–5.7 V for PMOS were applied to determine the time to breakdown at these voltages. The results fall on the same line as the voltage acceleration determined in the longer time-scale. In addition,  $V_{BD}$  determined from the ramped voltage measurements is in agreement with these points if we consider the bulk of the stress to have occurred in the final 100 ns step of the ramp and assign a time to breakdown of 100 ns. The PFET has a higher  $V_{BD}$  than the NFET in this voltage range due to the lower tunneling current at a given  $|V|$ . As shown, the voltage acceleration rules used for the DC case are applicable to the nanosecond measurements.

#### 4.2. Area-dependence for nanosecond measurements

The area-dependence is analyzed in Table 1. Using a Weibull shape factor of 1.2 obtained from DC measurements for this technology and in agreement with Fig. 4, we calculated the  $V_{BD}$  we would expect for a device with 10 times larger area. For the NFET the calculated values are very close to the measured values. For the PFET, the calculated difference between the two areas, 0.25 V, is similar to the measured difference of 0.26 V. Therefore, area scaling methods have been shown to apply to the nanosecond regime. With the use of thin oxides where gate oxide rupture must be carefully avoided during an ESD event, accurate calculation of the breakdown

Table 1  
Comparison of TLP measurements with calculations based on DC measurements for both *N* and PFETs

	TLP exp. from Fig. 8		DC Time to Breakdown data		Predicted from DC	
	1	2	3	4	5	6
Device	Median $V_{BD}$ from TLP for $0.13 \times 100 \mu\text{m}^2$ (Volts)	Meas. $V_{BD}$ from TLP for $0.13 \times 1000 \mu\text{m}^2$ (Volts)	Voltage acceleration (decades/V)	$t_{BD}$ from DC meas (sec.)	Calc. $V_{BD}$ for $0.13 \times 100 \mu\text{m}^2$ (Volts)	Calc. $V_{BD}$ for $0.13 \times 1000 \mu\text{m}^2$ (Volts)
NFET	$4.77 \pm 0.3$	$4.66 \pm 0.3$	$5.8 \pm 0.7$ near 3.6 V	0.084 at $V1 = 3.8$ V	$V2 = 4.8 \pm 0.2$	$V3 = 4.7 \pm 0.2$
PFET	$-5.93 \pm 0.3$	$-5.67 \pm 0.3$	$4.4 \pm 0.7$ near -4 V to $3.4 \pm 0.4$ near -5.5 V	0.19 at $V1 = -4.0$ V	$V2 = -5.8 \pm 0.3$	$V3 = -5.55 \pm 0.3$

Columns 1 and 2 are obtained from Fig. 8. Columns 3 and 4 are obtained from Fig. 9, although the PFET includes the curvature at higher voltages [13]. Columns 5 and 6 are calculated from the other columns using the following equations: (Column 5: using Volt. Acc. from Column 3,  $t_{BD1}$  and  $V1$  from Column 4, and  $t_{BD2} \sim 25\text{--}100$  ns,  $V2 = V1 + (1/\text{Volt. Acc.}) \times \log(t_{BD1}/t_{BD2})$ ) and (Column 6: using Volt. Acc. from Column 3 and  $\beta = 1.2$ ,  $V3 = V2 - (1/\text{Volt. Acc.}) \times (1/\beta) \log(A3/A2)$ ).

voltage, including area-dependence, is extremely important. If area considerations are neglected, as has been done in the past, 0.1–0.5 V errors can be made in  $V_{BD}$ .

#### 4.3. Thickness scaling

Dielectrics in NFETs ranging in thickness from 1.5 to 1.9 nm were tested in the DC regime and the nanosecond regime as shown in Fig. 10. In the DC regime, all were tested at 3.8 V and a thickness acceleration of 6.3 dec./nm was found. The physical thickness for the 1.7 nm and 1.9 nm dielectrics was determined by TEM analysis. The physical thickness of the 1.5 nm dielectric was estimated based on the measured differences in electrical thickness. In the ns regime, a ramped-voltage measurement was performed, and the slope of the median breakdown voltage vs. dielectric thickness was found to be 1.9 V/nm. Combining the two plots, we obtain a voltage acceleration of 3.3 dec./V, which is in agreement with the universal voltage acceleration curve shown in Fig. 2b. These data again demonstrate that the breakdown physics remains the same in the ns regime and that the parameters obtained from DC measurements can be used to extrapolate to the time-scale of interest for ESD events.

#### 4.4. Series resistance

One of the common techniques used to protect a sensitive device from snapback-induced failure is to add extra resistance between the ESD protection device and the device being protected. The resistor,  $R$ , is typically 10–200  $\Omega$  and it limits the current flowing into the device being protected. For example, if the ESD protection device has a resistance of 1  $\Omega$  during an ESD discharge, and the resistor  $R$  is 100  $\Omega$ , then only

1/100th of the total ESD discharge current could flow into the device being protected. For a 2 kV HBM discharge, the maximum current the device being protected will see is <13.3 mA. If the device failure current,  $I_{t2}$ , is larger than 13.3 mA then the device will be safe from ESD damage. A typical  $I_{t2}$  value for a 0.13  $\mu\text{m}$  NMOS is  $\sim 1$  mA/ $\mu\text{m}$  of transistor channel width, so this is a very effective method to enhance the ESD protection. However, the resistance of a gate dielectric is in the k $\Omega$  range, and it requires much less power to damage. Therefore, it will take a much larger  $R$  to limit the ESD current and power flowing into the device being protected to a safe level. Fig. 11 shows the median breakdown voltage as a function of the additional series resistance. In the case of 1.5 nm oxynitride breakdown, the traditionally used values of 100  $\Omega$  series resistance do not substantially alter the breakdown voltage. The 1 k $\Omega$  resistor does increase the breakdown voltage to 6.3 V. For all of the  $0.13 \times 100 \mu\text{m}$  area dielectrics tested without intentional series resistance, the average resistance value obtained from the TLP current and voltage immediately prior to breakdown was 3.2 k $\Omega$ . An additional 1 k $\Omega$  is therefore predicted to break down at a voltage given by  $4.77 \times 4.2/3.2$  dividing the voltage between the dielectric and the additional resistor. The result of 6.26 V is in close agreement with the experimental result of 6.33 V.

## 5. Implications

### 5.1. Projection to thinner dielectrics

Using all of this information, a projection can be made to a thinner dielectric. Although, gate dielectric reliability of PFETs is worse than that of NFETs below

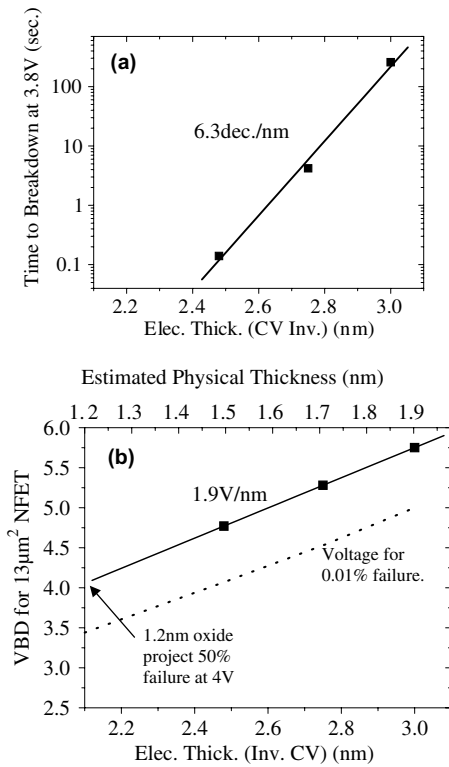


Fig. 10. (a) DC measurements of median time to breakdown vs. electrical thickness for NFETs with oxynitride gate dielectrics. All measurements were at 3.8 V and were either measured on or projected to 13  $\mu\text{m}^2$  device area; (b) TLP measurements of breakdown voltage for 13  $\mu\text{m}^2$  device area vs. electrical thickness. The top axis shows the physical oxide thickness corresponding to the electrical thickness measured by *CV* in inversion. The solid squares represent the median breakdown voltage and the dotted line represents the calculated voltage for 0.01% failure. TEM measurements are compared to electrical measurements for the 1.7 and 1.9 nm oxynitrides and the relationship is used to determine the physical thickness for the 1.5 nm structure.

$\sim 3$  V, NFET gate dielectrics are clearly more sensitive, in the region of interest for ESD events, as shown in Fig. 9. Therefore our projections will be for NFETS. Assuming that the thickness acceleration obtained in the 1.5–1.9 nm regime is valid down to 1.2 nm, as shown in Fig. 10, the median breakdown voltage for a 100 ns stress is projected to be 4 V for a 13  $\mu\text{m}^2$  device. The dotted line in the figure shows the voltage at which we would predict 0.01% failure. Eq. (2) is used to obtain this line. The Weibull slope from Fig. 4 and the voltage acceleration from Fig. 2b are used. The Weibull slope becomes shallower for thinner dielectrics, but is offset by the steeper voltage acceleration at lower voltages. The result of the calculation is that the voltage across the oxide must be kept below 3.4 V for a 13  $\mu\text{m}^2$  area

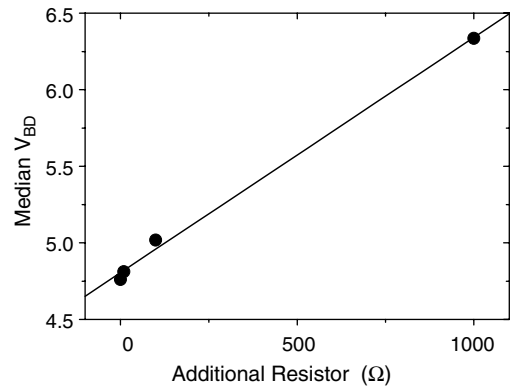


Fig. 11. TLP testing results from testers which included a series resistor in the layout. The median of >10 devices is shown for each resistor value.  $0.13 \times 100 \mu\text{m}$  NFETs with 1.5 nm oxynitrides were stressed with 100 ns TL pulses and 0.1 V steps.

in order to keep oxide breakdown below the 100 ppm level.

## 6. Conclusions

We have reviewed important concepts for oxide breakdown, such as the anode–hole injection model, the area and statistical dependence of breakdown and soft breakdown. We have shown that projections of dielectric breakdown from DC measurements are in agreement with nanosecond measurements of hard breakdown and that the breakdown transient can take less than 2 ns. With the knowledge that breakdown in the nanosecond regime follows the well-understood voltage acceleration, area-dependence and thickness dependence, we can expect that the Weibull statistics are obeyed as well and dielectric breakdown can be fully included in ESD design using standard extrapolation techniques.

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