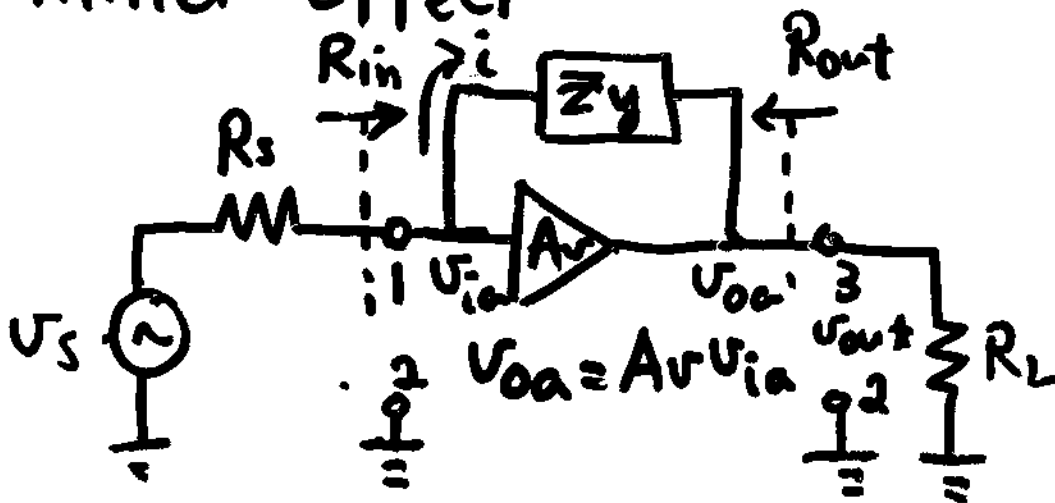


Miller Effect



$$R_{in} = \frac{V_{ia}}{i}$$

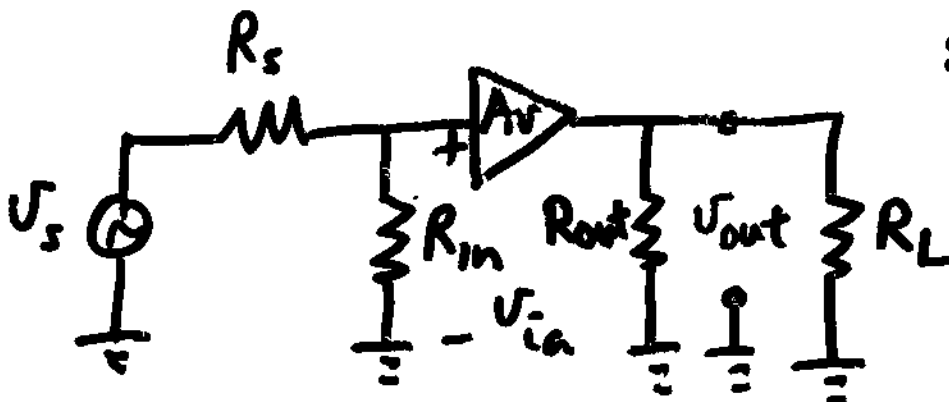
$$i = \frac{V_{ia} - V_{oa}}{Z_y} = \frac{V_{ia} - A_v V_{ia}}{Z_y}$$

$$= \frac{(1 - A_v) V_{ia}}{Z_y}$$

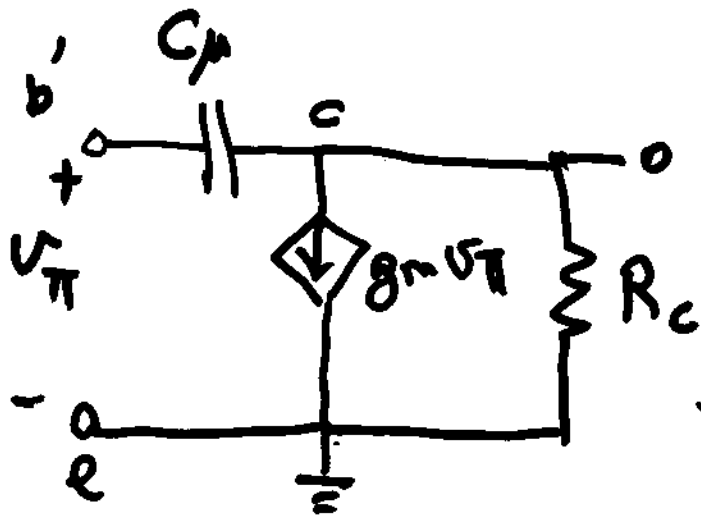
$$R_{in} = \frac{Z_y}{1 - A_v}$$

$$R_{out} = \frac{Z_y}{1 - \frac{1}{A_v}}$$

$$\approx Z_y$$



For large $|A_v|$



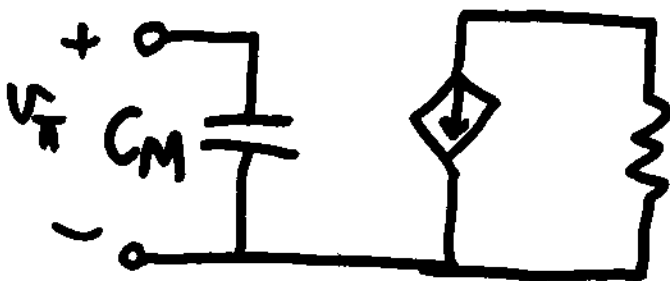
$$\frac{v_o}{v_{in}} = \frac{-g_m v_{\pi} R_c}{v_{\pi}} = -g_m R_c$$

$$v_c = -g_m v_{\pi} R_c$$

$$v_{b'e} = v_{\pi} (1 + g_m v_{\pi} R_c)$$

Charge supplied to C_{μ}

$$Q_1 = C_{\mu} v_{b'e} = C_{\mu} v_{\pi} (1 + g_m R_c)$$



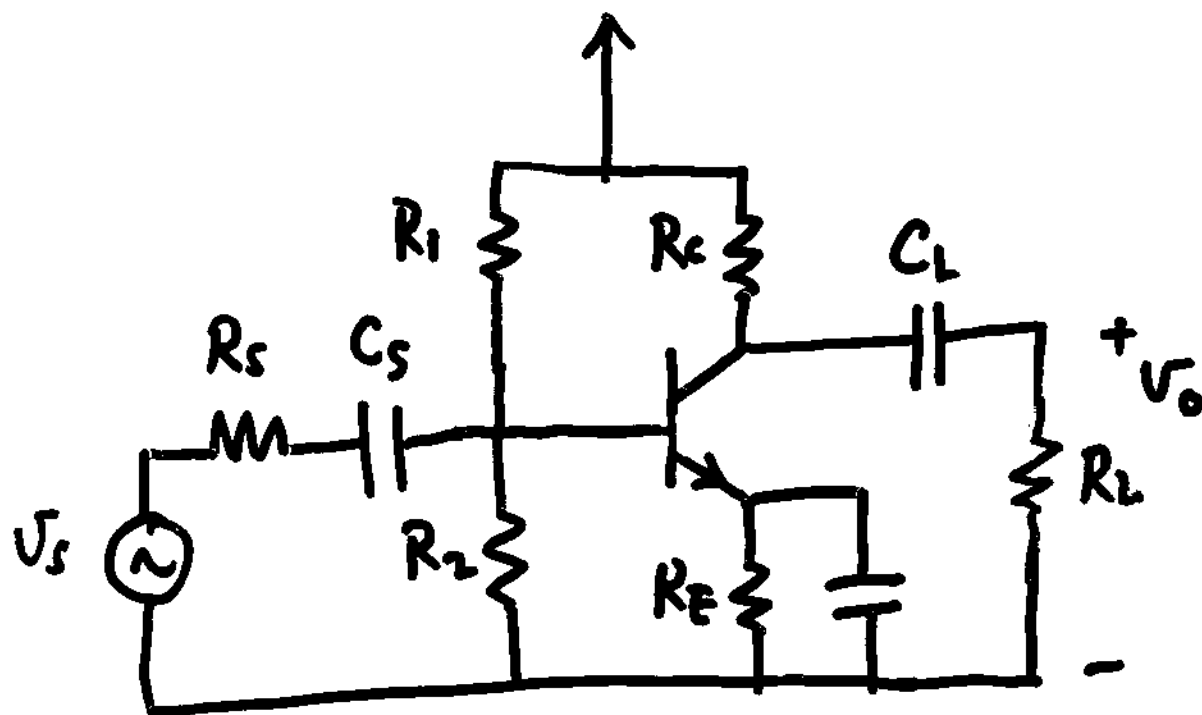
Charge supplied to C_M

$$Q_2 = C_M v_{\pi}$$

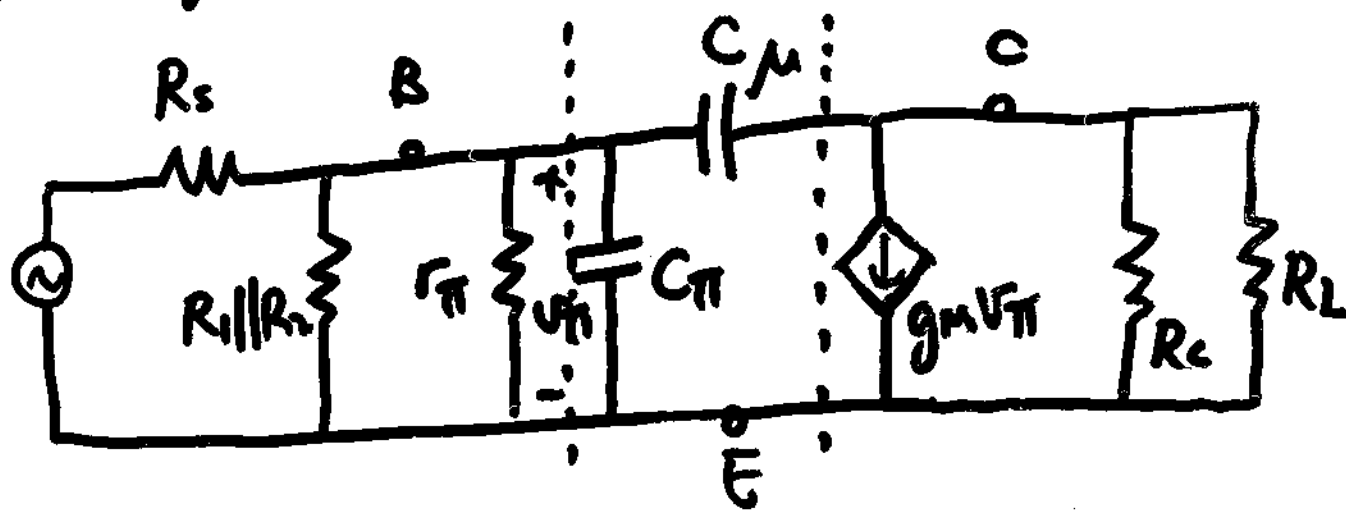
$$Q_1 = Q_2 \Rightarrow C_M = (1 + g_m R_c) C_{\mu}$$

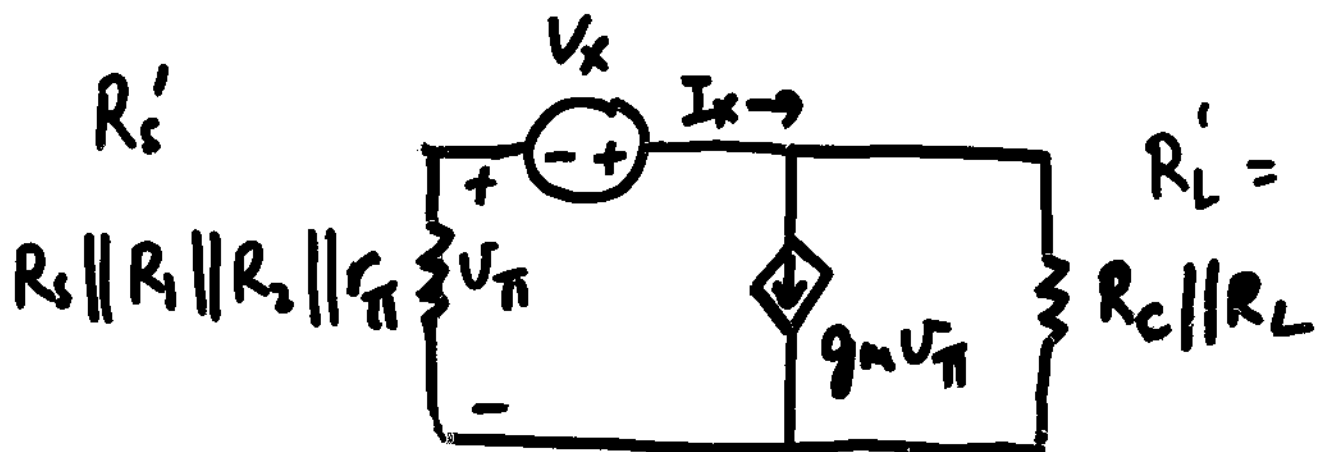
Unilateral equivalent ckt

High Frequency CE Amplifier



High-freq equiv. ckt





$$V_x = [I_x + g_m I_x R_s'] R_L' + I_x R_s'$$

$$\Rightarrow R_{\mu} = (1 + g_m R_s') R_L' + R_s'$$

$$= R_s' (1 + g_m R_L') + R_L'$$

$$\tau_{\mu} = R_s' (1 + g_m R_L') C_{\mu} + R_L' C_{\mu}$$

$$\underbrace{(1 + g_m R_L')}_{(1 - A_v)} C_{\mu} = C_M$$

$$R_{\pi} = R_s'$$

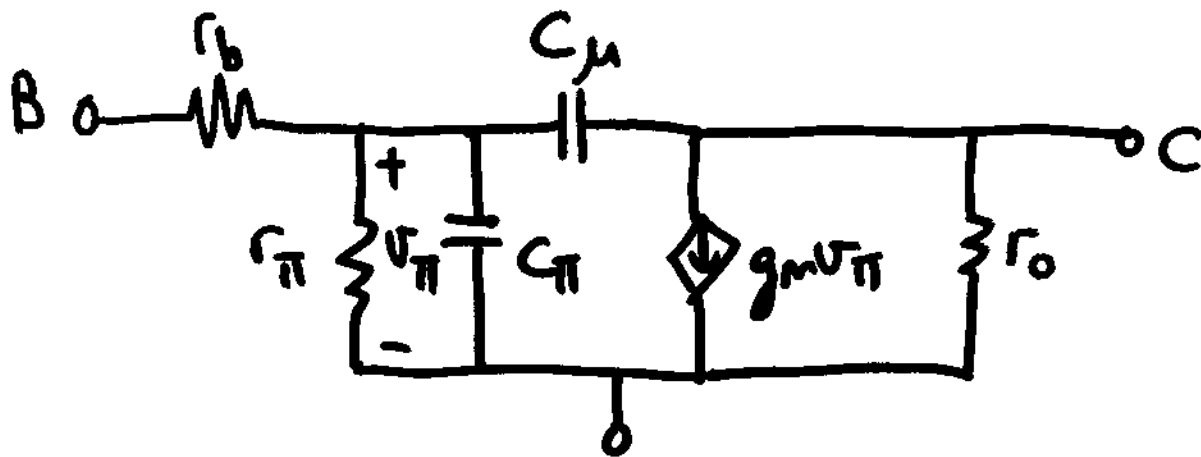
$$\tau_{\pi} = R_s' C_{\pi}$$

$$\omega_H \cong \frac{1}{\tau_{\pi} + \tau_{\mu}}$$

Short-circuit current gain

Manufacturer specifies cut-off frequency or unity-gain bandwidth

f_T

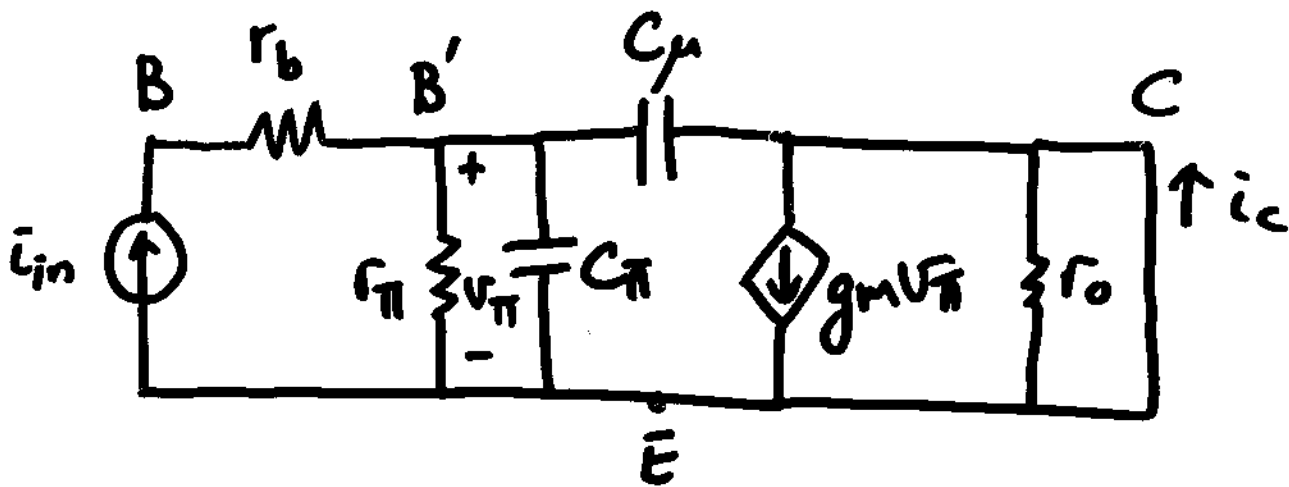


Low ω : C_μ, C_π open
current flows through r_π , leading to v_π , high $g_m v_\pi$ current

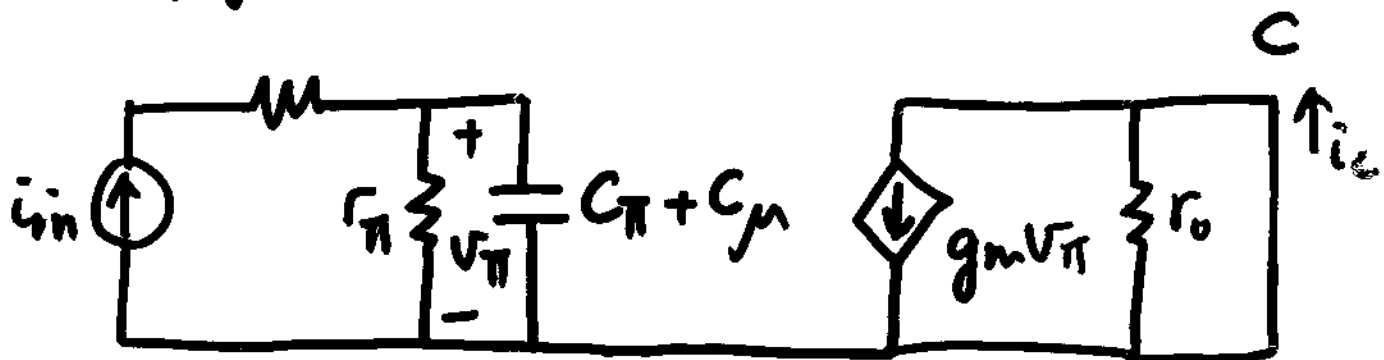
High ω : C_μ, C_π look more like short ckt
less current through r_π ,
less $g_m v_\pi$ current

Dependence of β on ω

Short C, use a current source input



$$A_v = 0$$

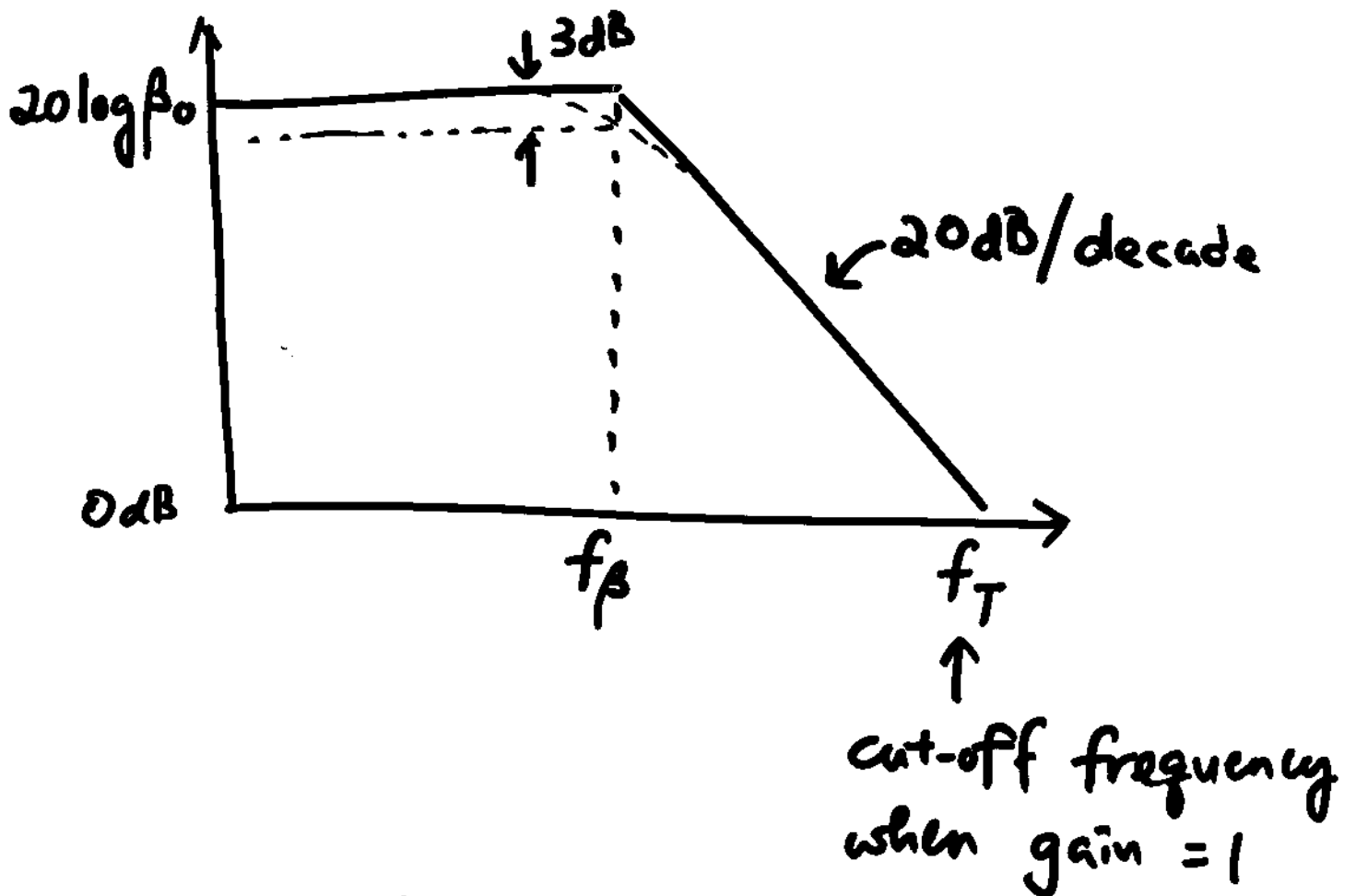


$$v_{\pi} = i_{in} \frac{r_{\pi}}{1 + j\omega r_{\pi} (C_{\pi} + C_{\mu})}$$

$$i_c = g_m v_{\pi}$$

(h_{fe}) Current gain $\frac{i_c}{i_{in}} = \frac{\beta_0}{1 + j\omega r_{\pi} (C_{\pi} + C_{\mu})}$

f_{β} , β -cutoff frequency (3dB drop) $= \frac{1}{2\pi r_{\pi} (C_{\pi} + C_{\mu})}$



$$20 \log \frac{f_T}{f_\beta} = 20 \log \beta_0 \quad \begin{array}{l} \text{unity-gain} \\ \text{bandwidth} \\ \text{or} \end{array}$$

$$f_T = f_\beta \beta_0 \leftarrow \text{gain-bandwidth product}$$

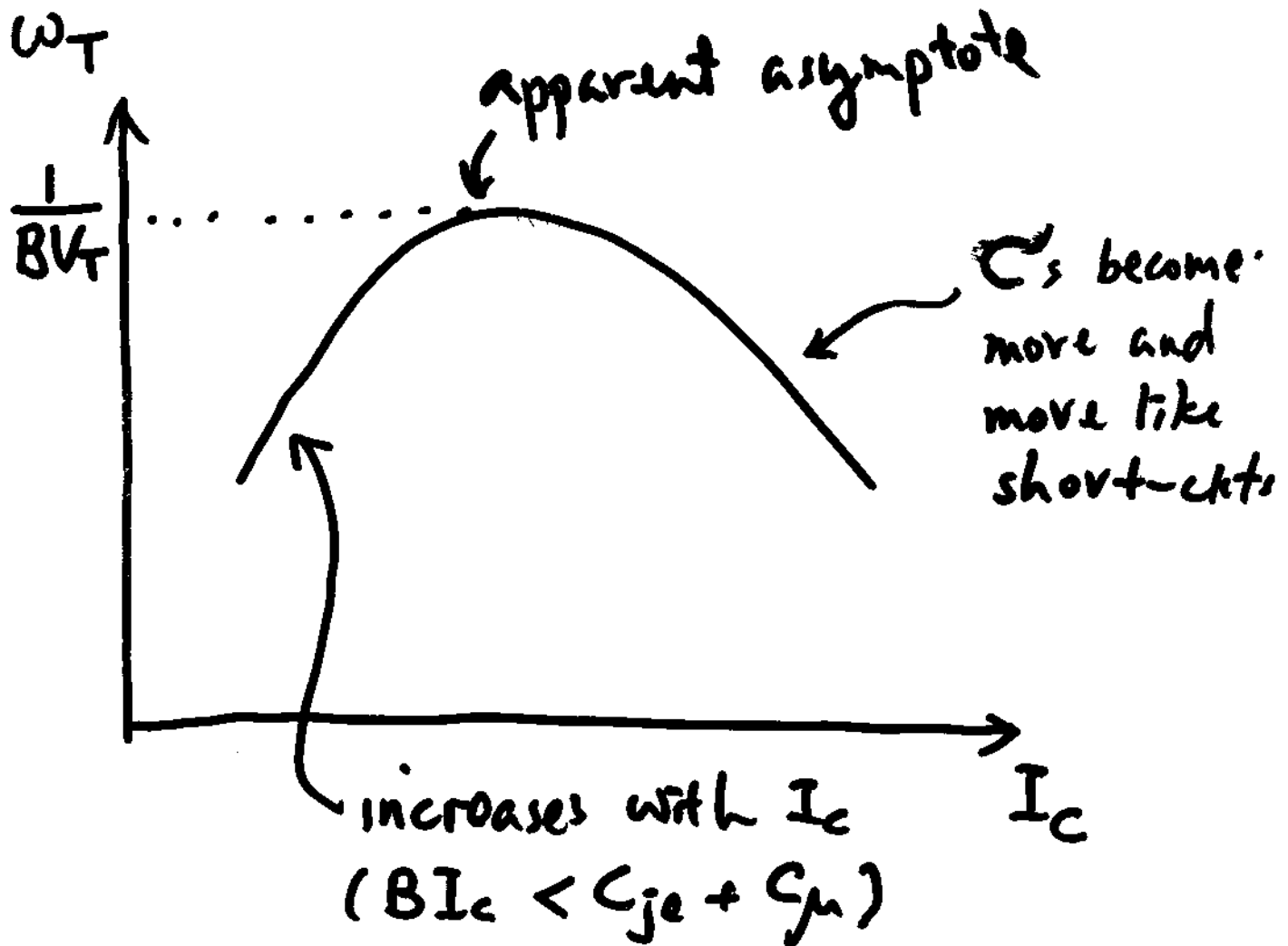
$$= \frac{\beta_0}{2\pi r_\pi (C_\pi + C_\mu)}$$

$$= \frac{g_m}{2\pi (C_\pi + C_\mu)}$$

f_T given by manufacturer

F_T vs. I_C

$$\begin{aligned}\omega_T &= \frac{g_m}{C_{\pi} + C_{\mu}} \\ &= \frac{g_m}{C_{je} + \beta I_C + C_{\mu}} \\ &= \frac{I_C}{V_T (C_{je} + \beta I_C + C_{\mu})}\end{aligned}$$



Example

$$\beta_0 = 200$$

$$\omega_T = 500 \cdot 10^6 \text{ rad/s}$$

$$n = 1$$

$$V_{bi} = 0.8 \text{ V}$$

$$V_{BE(on)} = 0.65 \text{ V}$$

$$C_{\mu} = 3 \text{ pF}$$



a) Find g_m , r_{π} , C_{π} , ω_{β} if $I_C = 1 \text{ mA}$
 $V_{CE} = 10 \text{ V}$

$$g_m = \frac{I_C}{V_T} = 38.5 \text{ mA/V}$$

$$r_{\pi} = \frac{\beta}{g_m} = 5.2 \text{ k}\Omega$$

$$C_{\pi} = \frac{g_m}{\omega_T} - C_{\mu} = 74 \text{ pF}$$

$$\omega_{\beta} = \frac{1}{r_{\pi}(C_{\pi} + C_{\mu})} = 2.5 \text{ M rad/s}$$

b) If $I_c = 2\text{mA}$, $V_{ce} = 5\text{V}$?

g_m doubles

r_{π} halved

$$C_{\mu} = \frac{C_{j0}}{\left(1 + \frac{V_{CB}}{V_{bi}}\right)^N} \quad \frac{1}{3} < N < \frac{1}{2}$$

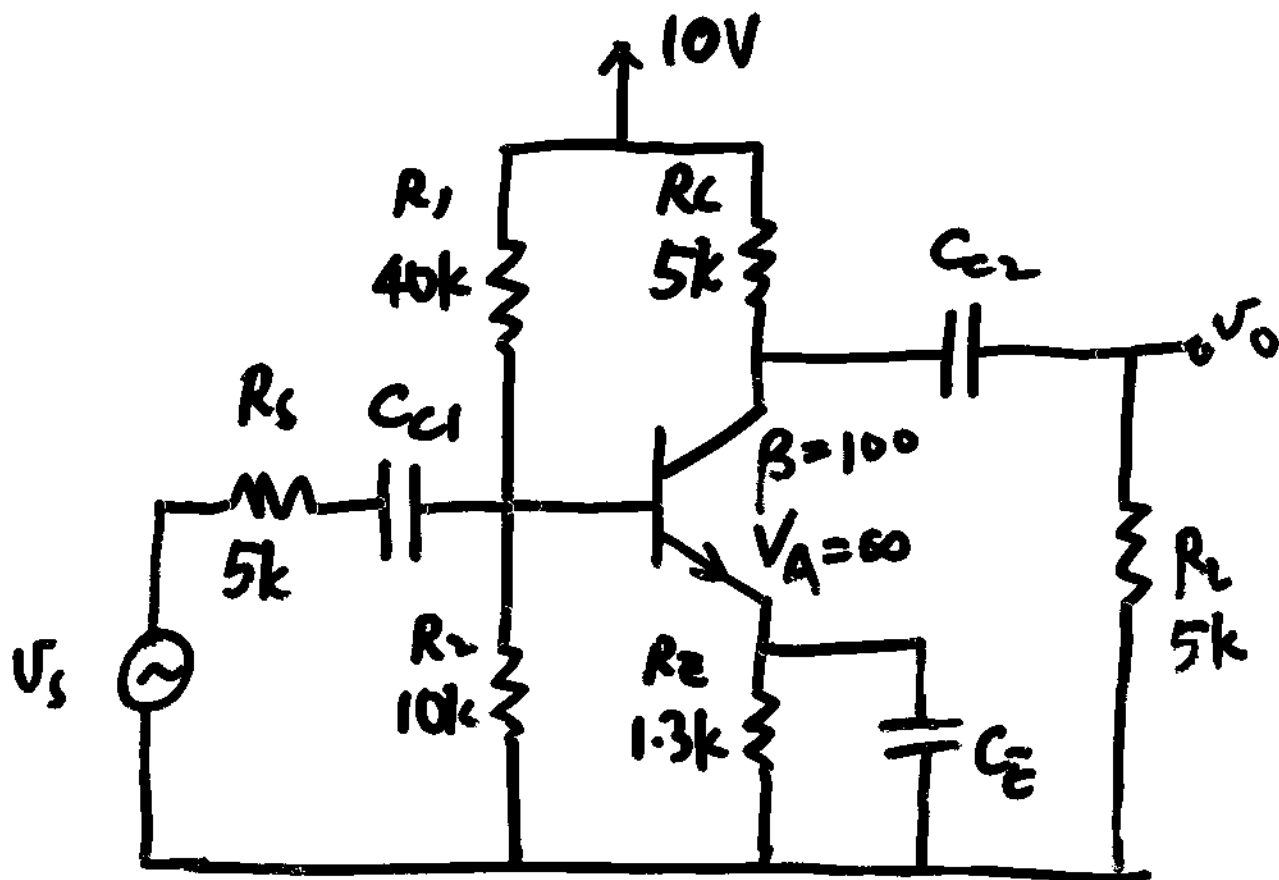
$$\frac{C_{\mu 1}}{C_{\mu 2}} = \frac{\left(1 + \frac{4.35}{0.8}\right)^N}{\left(1 + \frac{9.35}{0.8}\right)^N} = \frac{3\text{pF}}{C_{\mu 2}}$$

Assume $N = \frac{1}{2}$

$$C_{\mu 2} = 4.2\text{pF}$$

$$C_{\pi} = \frac{\omega_T}{g_m} - C_{\mu}$$
$$= 92\text{pF}$$

ω_T almost
doubles
 $\approx 800 \cdot 10^6 \text{ rad/s}$
(from data sheet)



$$V_{BE} = 0.7V$$

$$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E} = 9.33 \mu A$$

$$I_C = 0.933 \text{ mA}$$

$$I_E = 0.943 \text{ mA}$$

$$V_{CB} = 3.41V$$

$$C_{\mu} = \frac{C_{j0}}{\left(1 + \frac{V_{CB}}{V_{Bi}}\right)^{1/2}}$$

$$= 2 \text{ pF}$$

$$C_{j0} = 3.54 \text{ pF}, V_{Bi} = 0.75V$$

$$g_m = \frac{I_C}{V_T} = 35.9 \text{ mA/V}$$

$$r_{\pi} = \frac{V_T}{I_B} = 2.79 \text{ k}\Omega$$

$$C_{\mu} = 2 \text{ pF}$$

$$\text{given } f_T = 500 \text{ MHz}$$

$$C_{\pi} = \frac{g_m}{2\pi f_T} - C_{\mu} = 94 \text{ pF}$$

$$A_{MB} = -g_m (R_{C1} \parallel R_L) = -89.8$$

$$A_{v_s, MB} = A_{MB} \cdot \frac{R_1 \parallel R_2 \parallel r_{\pi}}{R_1 \parallel R_2 \parallel r_{\pi} + R_s} = -26.3$$

$$\begin{aligned} R_{\mu} &= (R_s \parallel R_1 \parallel R_2 \parallel r_{\pi})(1 - A_{MB}) + R_{C1} \parallel R_L \\ &= 1.46 \text{ k}\Omega (90.8) + 2.5 \text{ k}\Omega \\ &= 135 \text{ k}\Omega \end{aligned}$$

$$\tau_{\mu} = 270 \text{ ns}$$

$$\omega_H = \frac{1}{\tau_{\mu} + \tau_{\pi}}$$

$$R_{\pi} = 1.46 \text{ k}\Omega$$

$$= 3.52 \times 10^6 \text{ rad/s}$$

$$\tau_{\pi} = 13.7 \text{ ns}$$

$$f_H = 561 \text{ kHz}$$

Gain - Bandwidth Product of CE

$$\omega_H \cong \frac{1}{\tau_\mu} \cong \frac{1}{R_s' C_M}$$
$$\cong \frac{1}{R_s' |A_{MB}| C_\mu}$$

$$f_H \cong \frac{1}{2\pi R_s' |A_{MB}| C_\mu}$$

$$f_H \times |A_{MB}| = \frac{1}{2\pi R_s' C_\mu} \cong \text{constant}$$

independent of V_{CE}
or I_C

