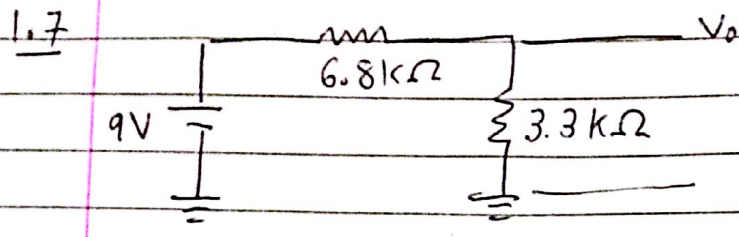
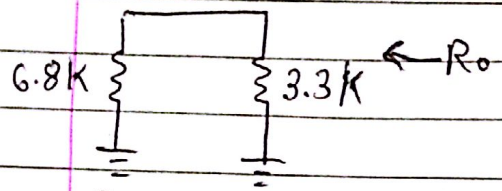


ECE 255 HW1 (Section 2)



$$V_o = \left(\frac{3.3}{3.3 + 6.8} \right) 9$$

$$= 9 \left(\frac{3.3}{10.1} \right) = 2.94V$$



$$R_o = (3.3 \parallel 6.8) k\Omega = 2.22 k\Omega$$

For $\pm 5\%$ Resistor tolerance, $V_o - low = 9 \left[\frac{3.3(1-0.05)}{3.3(1-0.05) + 6.8(1+0.05)} \right]$

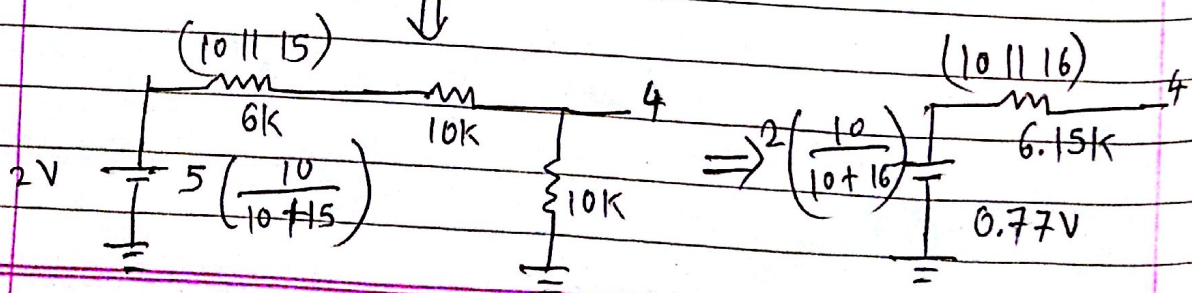
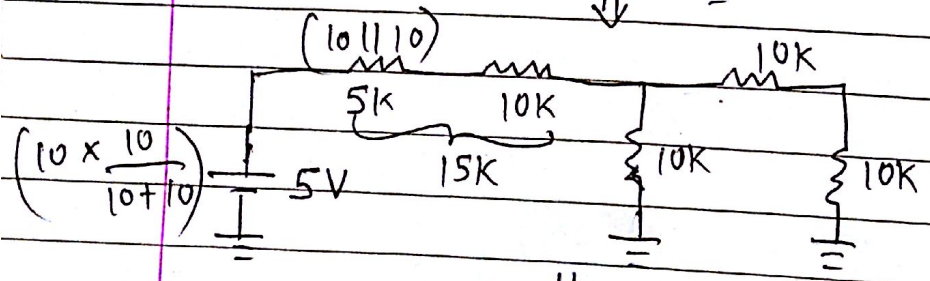
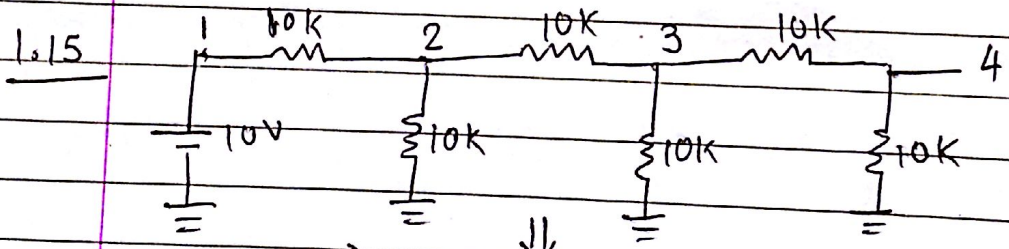
$$V_o - high = 9 \left[\frac{3.3(1+0.05)}{3.3(1+0.05) + 6.8(1-0.05)} \right] = 2.75V$$

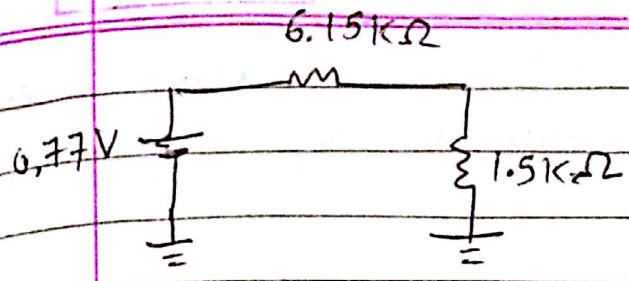
$= 3.14V$ V_o has a range of $2.75V$ to $3.14V$

$$R_o - low = \frac{3.3(1-0.05) \times 6.8(1-0.05)}{3.3(1-0.05) + 6.8(1-0.05)}$$

$$= 2.11 k\Omega$$

$$R_o - high = \frac{3.3(1+0.05) \times 6.8(1+0.05)}{3.3(1+0.05) + 6.8(1+0.05)} = 2.33 k\Omega$$



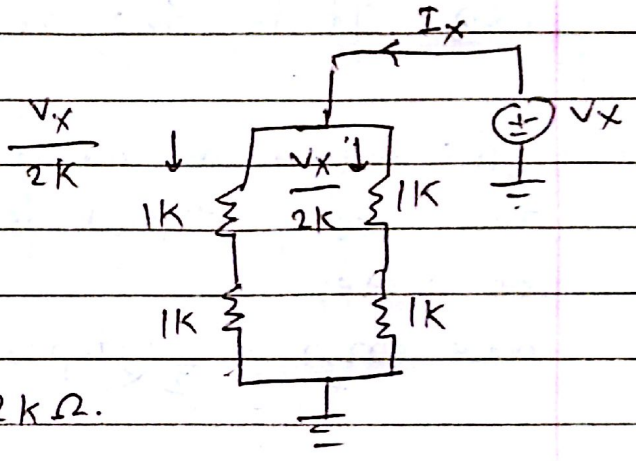


$$I = \frac{0.77}{6.15 + 1.5} = \underline{0.1 \text{ mA}}$$

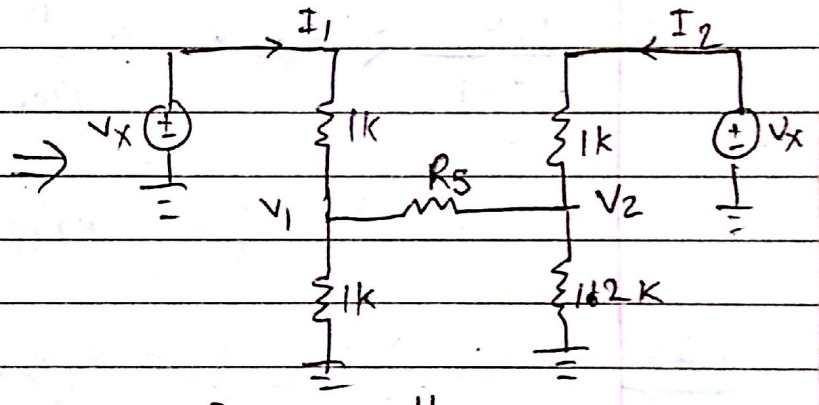
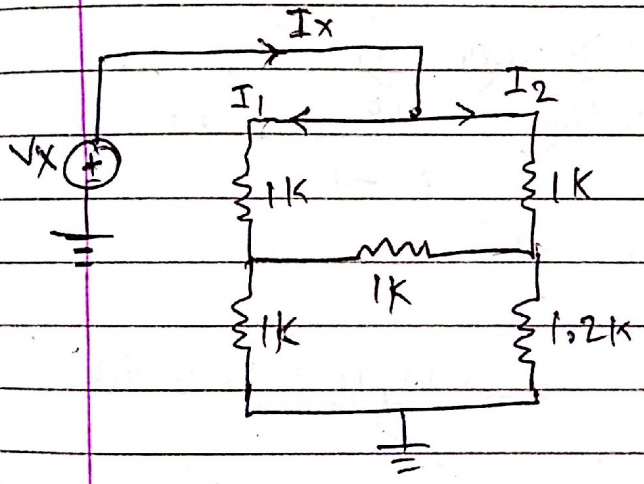
1.18 Due to symmetry in circuit, there will be no current in R_5 .

$$I_x = \frac{V_x}{2k} + \frac{V_x}{2k}$$

$$= \frac{V_x}{1k} \Rightarrow R_{eq} = \underline{1k\Omega}$$

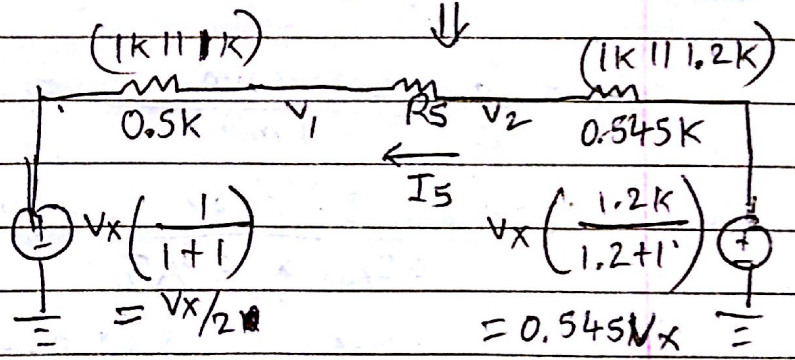


Now, R_4 is raised to $1.2k\Omega$.



$$I_5 = \frac{0.545 V_x - 0.5 V_x}{0.5 + 1 + 0.545}$$

$$= 0.022 V_x$$



$$V_1 = \frac{V_x}{2} + 0.022 V_x \times 0.5 = 0.511 V_x$$

$$V_2 = V_1 + I_5 R_5 = 0.533 V_x$$

$$I_1 = \frac{V_x - V_1}{1k} = 0.489 V_x, \quad I_2 = \frac{V_x - V_2}{1k} = 0.467 V_x$$

$$I_x = I_1 + I_2 = 0.956 V_x \Rightarrow R_{eq} = \frac{V_x}{I_x} = \underline{1.05k\Omega}$$

1.36 (a) For N bit ADC, there will be 2^N possibilities (levels) from 0 to VFS. So, $(2^N - 1)$ possible steps with step size given by $\frac{VFS}{2^N - 1}$

This is analog change corresponding to a change in LSB. It is the resolution of ADC.

(b) The maximum error occurs when the analog signal is at the middle of a step.

$$\text{max error} = \frac{1}{2} (\text{step size}) = \frac{1}{2} \frac{VFS}{2^N - 1}$$

called quantization error

(c) $\frac{10V}{2^N - 1} \leq 5 \text{ mV} \Rightarrow 2^N - 1 \geq 2000 \Rightarrow N = 11$
 Resolution = $\frac{10}{2^{11} - 1} = 4.9 \text{ mV}$

$$\text{Quant. error} = \frac{4.9}{2} = 2.4 \text{ mV}$$

1.40 $A_v = \frac{V_o}{V_i} = \frac{2.2}{0.2} = 11 \text{ V/V}$ or $20 \log 11 = 20.8 \text{ dB}$

$$A_i = \frac{i_o}{i_i} = \frac{2.2 \text{ V} / 100 \Omega}{1 \text{ mA}} = 22 \text{ A/A}$$
 or $20 \log A_i = 26.8 \text{ dB}$

$$A_p = \frac{P_o}{P_i} = \frac{(2.2/\sqrt{2})^2 / 100}{0.2/\sqrt{2} \times 10^{-3} / \sqrt{2}} = 242 \text{ W/W}$$
 or $10 \log A_p = 23.8 \text{ dB}$

Supply power = $2 \times 3 \text{ V} \times 20 \text{ mA} = 120 \text{ mW}$

output power = $\frac{V_{rms}^2}{R_L} = \frac{(2.2/\sqrt{2})^2}{100 \Omega} = 24.2 \text{ mW}$

input power = $\frac{24.2}{242} = 0.1 \text{ mW}$ (negligible)

amplifier dissipation = supply power - output power
 $= 120 - 24.2 = 95.8 \text{ mW}$

amplifier efficiency = $\frac{O.P.}{i.p.} \times 100 = \frac{24.2}{120} \times 100 = 20.2\%$