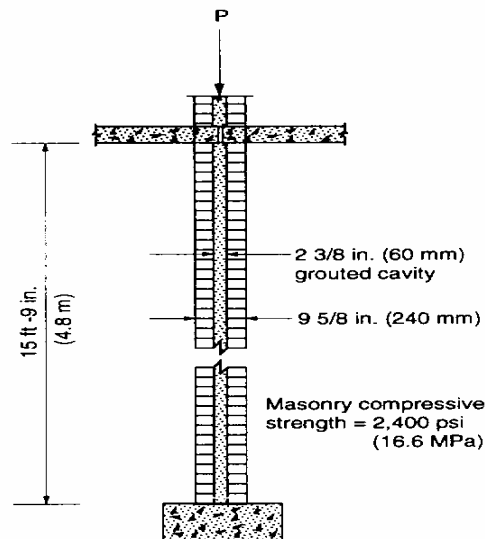


Ce 479
 Homework 2 (Unreinforced Masonry using Allowable Stresses)
 Fall 2006
 Solution: JAR

1. For the wall of Problem #1, determine the allowable design axial load, P, according to the ACI 530 -Allowable Stress Provisions. The wall is fully grouted.

Solution: The wall is fully grouted to act as a unit. The prisms have been tested and the masonry compressive strength is 2400 psi. The load is concentrically applied along the length of the wall. Assuming pinned ends, determine h/r, where h is the wall height and r is the radius of gyration:



$$\begin{aligned}
 h &:= 15.75 \cdot 12 & I &:= 9.625 \cdot 9.625 \cdot 9.625 \cdot \frac{12}{12} & I &= 891.666 \text{ in}^3/\text{ft} \\
 h &= 189 \text{ inches} & A_{net} &:= 9.625 \cdot 12 & A_{net} &= 115.5 \text{ in}^2/\text{ft} \\
 r &:= \sqrt{\frac{I}{A_{net}}} & r &= 2.778 \text{ inches} & \frac{h}{r} &= 68.022
 \end{aligned}$$

Since h/r is less than 99, the failure load is overestimated by the buckling equation, (2-15). The empirical relationship, (2-12), best fits the available test results with a factor of safety of 4.0.

$$\begin{aligned}
 f_m &:= 2400 \text{ psi} \\
 F_a &:= 0.25 \cdot f_m \cdot \left[1 - \left(\frac{h}{140 \cdot r} \right)^2 \right] & F_a &= 458.356 \text{ psi}
 \end{aligned}$$

$$P_{all} := F_a \cdot A_{net}$$

$$P_{all} = 52940 \text{ lbs}$$

The wall stability must also be checked:

$$E := 700 \cdot f_m \quad E = 1.68 \times 10^6 \text{ psi}$$

$$P_e := 9.86 \cdot E \cdot \frac{I}{h^2} \quad P_e = 413490 \text{ lbs}$$

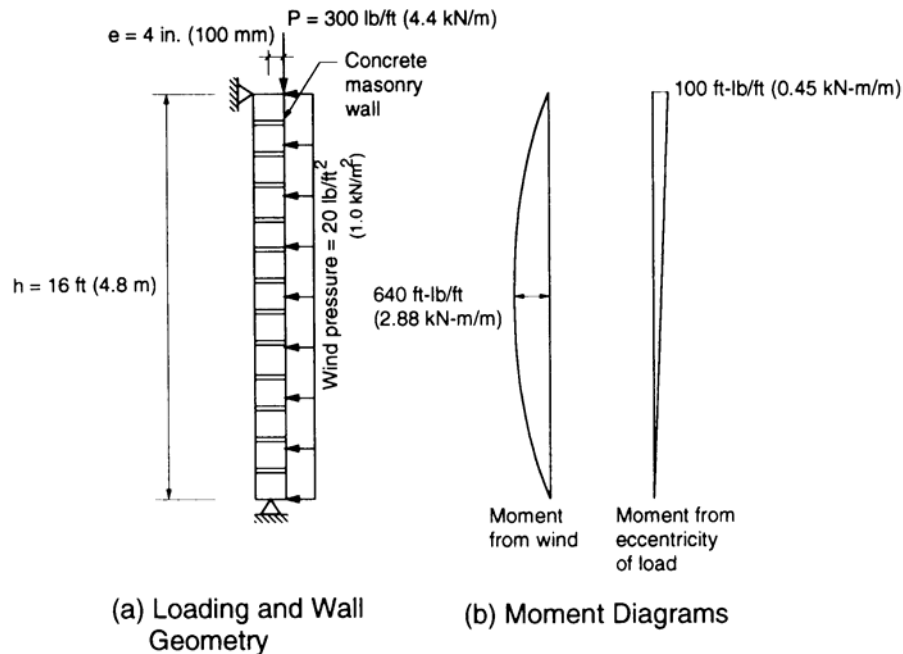
$$P_{max} := \frac{P_e}{4} \quad P_{max} = 103372 \text{ lbs, which greater than the allowable. Thus OK!}$$

2. Design the concrete block wall to carry a vertical load of 300 lb/ft with a 4-inch eccentricity in addition to a lateral load of 20 lb/ft². The wall is 16 ft high and is simply supported at the top and at the bottom as shown in the figure. The wall is built with 8-inch CMU and face shell bedding of portland cement type S mortar. The self-weight of the wall is 720 lb/lineal ft of wall. If the current thickness is not adequate in accordance with ACI 530-Allowable Stresses, increase it to a 12-inch CMU (net 11.625 inches, wall self-weight of 1024 lb/lineal ft of wall) with a 1.5 inch face shell bedding. Use a compressive strength for masonry of 2000 psi.

The approach is to check two load conditions, (1) Gravity load and no wind- the critical section is located at the top of wall, and (2) Gravity load plus wind- the critical section is located at mid-height of the wall.

1) Gravity load check:

i) compression controls



$$f_{m2} := 2000 \text{ psi}$$

$$P_{ax} := 300 \text{ lbs/ft} \quad A_{net2} := 2 \cdot 1.25 \cdot 12 \quad A_{net2} = 30 \text{ in}^2/\text{ft}$$

$$M := 100 \cdot 12 \quad M = 1.2 \times 10^3 \text{ in-lb} \quad S_2 := 81 \text{ in}^3/\text{ft}$$

$$f_{a2} := \frac{P_{ax}}{A_{net2}} \quad f_{a2} = 10 \text{ psi} \quad f_{b2} := \frac{M}{S_2} \quad f_{b2} = 15 \text{ psi}$$

$$h_2 := 16 \cdot 12 \quad h_2 = 192 \text{ in} \quad I_2 := 309 \text{ in}^4/\text{ft} \quad r_2 := \left(\frac{334}{41.5} \right)^{\frac{1}{2}}$$

$$r_2 = 2.837 \text{ in/ft} \quad \frac{h_2}{r_2} = 68 \quad \text{this is less than 99.}$$

$$F_{a2} := 0.25 \cdot f_{m2} \cdot \left[1 - \left(\frac{h_2}{r_2 \cdot 140} \right)^2 \right] \quad F_{a2} = 383 \text{ psi}$$

$$F_{b2} := 0.3 \cdot f_{m2} \quad F_{b2} = 600 \text{ psi}$$

$$\left(\frac{f_{a2}}{F_{a2}} \right) + \left(\frac{f_{b2}}{F_{b2}} \right) = 0.051 \quad \text{less than 1.0 therefore, OK.}$$

Check wall stability: $E_2 := 900 \cdot f_{m2} \quad E_2 = 1.8 \times 10^6 \text{ psi}$

$$P_{e2} := 9.86 \cdot E_2 \cdot \frac{334 \cdot \left[1 - 0.577 \cdot \left(\frac{4}{r_2} \right) \right]^3}{h_2^2} \quad P_{e2} = 1.042 \times 10^3 \text{ lbs}$$

Since $P_{e2}/4 = 260 \text{ lbs} < 300 \text{ lbs}$, therefore N.G. Thus, try 12 inch CMU

ii) Tension limit:

$$f_{a2} - f_{b2} = -5 \text{ psi, tension} < F_t, \text{ where } F_t = 25 \text{ psi from Table 2.2.3.2}$$

2. Check gravity load plus wind case with critical section at mid-height of the wall.
Maximum moment due to wind is 640 lb-ft

$$M_{\max gw} := 640 + 50 \quad M_{\max gw} = 690 \quad \text{ft-lb}$$

$$f_{bgw2} := \frac{M_{\max gw} \cdot 12}{S2} \quad f_{bgw2} = 102 \quad \text{psi}$$

$$f_{agw2} := 10 + \frac{720 \cdot 0.5}{31} \quad f_{agw2} = 22 \quad \text{psi}$$

i) Tension control $f_{agw2} - f_{bgw2} = -81 \text{psi}$. The wall is in tension!! N.G.
Thus, try 12 inch block

ii) Compression control

$$\left(\frac{f_{agw2}}{F_{a2}} \right) + \left(\frac{f_{bgw2}}{F_{b2}} \right) = 0.227$$

Therefore, OK for compression but wall thickness must be increased due to inadequate tension capacity and stability